

THEORETICAL AND EXPERIMENTAL ANALYSIS OF T-JOINT IN TIG WELDING PROCESS

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ABSTRACT- Arc welded structures are extensively used in automobiles, constructions and power plants. As the main cause of weldment failure is design defect and overload, hence it is necessary to analyze the maximum stresses in the weldment. In this work deals with investigation of welded T-joint by TIG welding process with varying gap and angle between the parent material to determine the breaking stress under tensile load in the weldment. Finite element analysis used to carried out the maximum breaking stress using Ansys software. Experimental analysis used to carried out the maximum breaking stress under tensile load. Taguchi optimization method used to optimize the fillet weld section in experimental analysis. Angle, arc force and gap between parent materials are the three process parameters used for the taguchi optimization technique. The FE analysis & analytical results of breaking

stress is also carried out and verified with the experimental result. The optimized best fillet weld section (low carbon steel AISI1020 and copper) is carried out and used to restrict the weldment failure.

Keywords: Arc welded structure, Weldment failure, Taguchi optimization, low carbon steel AISI1020, Copper

1.INTRODUCTION

The fillet welded joints commonly suffer from various welding deformation patterns, such as, angular distortion, longitudinal & transverse shrinkage in fabrication of structural members in shipbuilding, automobile and other industries that angular distortion defined through numerical calculation[1-3]. The stresses in the weldment are evaluated by varying the gap between the base plates which may occur during manufacturing[4]. It is distinguished from other forms of mechanical connection, such as riveting or bolting, which are formed by friction or mechanical interlocking. It is one of the oldest and reliable methods of joining[5]. The residual stress in a welded T-joint, comparing those computed by 3D models with those computed by 2D models[6].

A mathematical model for predicting weld penetration as a function of welding process variables. The constrained optimization method is then applied to this model to optimize process variables for maximizing weld penetration [7-9]. Welding offers many advantages over bolting and riveting. Welding enables direct transfer of stress between members eliminating closure and splice plates necessary for bolted structures. Hence, the weight of the joint is minimum. Generally welded joints are as strong as or stronger than the base metal, thereby placing no restriction on the joints.

Some of the disadvantages of welding are that it requires skilled manpower for welding as well as inspection. Welding in the field may be difficult due to the location or environment. Welded joints are highly prone for cracking under fatigue loading large residual stresses and distortions are developed in welded connections.

2. NUMERICAL CALCULATION

2.1 WELDMENT UNDER TENSILE LOAD

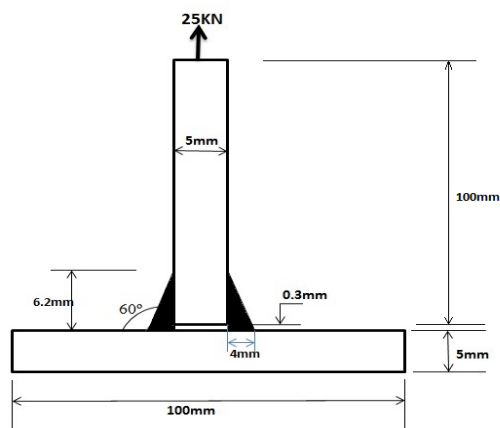


Fig. 2.1 Arc weld of T-joint under tensile load for 0.3mm gap and 60° angle

The above Fig 2.1 represents the T-joint fillet weld sections with dimensions (100x50x5mm) with fillet angle 45°. Here

25 KN tensile acting upward on the top of the section. The base weld material is plain carbon steel and filler material is copper (Cu).

T-joint fillet welds the dimensions are specified are as follows.

- F-Tensile load on vertical plate (N) = 25KN
- w-Leg length of weld (mm) = 4.0 mm
- h -Throat of fillet weld (mm)
- = w X [cos45°]
- l-Length of weld or size of weld (mm) = 50mm
- l_T-length of top load section = 5mm
- b_T-breath of top load section = 50mm
- l_t-throat length = 4mm
- t- throat thickness = 1mm
- A -Area of weld section

The material properties are specified are as follows,

- Modulus of elasticity of base plate material (E) = 2.1 x 10⁵MPa
- Poisson's ratio of base plate material (μ) = 0.3
- Modulus of elasticity of weld material (E) = 1.1 x 10⁵ MPa
- Poisson's ratio of weld material (μ) = 0.37

Formula used,

$$\text{Area of weld section}(A) = 2A_f + A_l - A_t$$

Where,

$$A_f - \text{Area of fillet section} = 2x(\cos\theta \times w) \times l$$

$$A_l - \text{Area of load section} = l_T \times b_T$$

$$A_t - \text{Throat area} = t \times l_t$$

Therefore,

Breaking stress = (Breaking Load(P)/Throat Area) X Stress Concentration Factor(k)

$$= \frac{P}{A_t} \times k$$

Stress concentration factor (k) parent material is the range of 3.5 to 4 given by Frank Karl Heinz [16].

2.2 BREAKING STRESS

The model calculation of breaking stress for tensile load with different angle and varying gap between parent materials given below,

1. 25KN load, $\theta = 45^\circ$ and 0.3 mm gap

$$\text{Breaking stress } (\sigma_b) = \frac{F}{A} \times k$$

$$\begin{aligned} A &= 2 A_f + A_1 - A_t \\ &= 2(\cos 45 \times 6.2 \times 50) + (5 \times 50) - (.3 \times 4) \\ &= 531.8 \text{ mm}^2 \\ &= \frac{25000}{531.8} \times 4 \end{aligned}$$

$$\sigma_b = 188.04 \text{ Mpa.}$$

2. 25KN load, $\theta = 60^\circ$ and 0.3mm gap

$$\begin{aligned} A &= 2(\cos 60 \times 4 \times 50) + (5 \times 50) - (0.3 \times 4) \\ &= 448.8 \text{ mm}^2 \\ &= \frac{25000}{448.8} \times 4 \end{aligned}$$

$$\sigma_b = 222.2 \text{ Mpa}$$

3. 25KN load, $\theta = 30^\circ$ and 0.3mm gap

$$\begin{aligned} A &= 2(\cos 30 \times 4 \times 50) + (5 \times 50) - (.3 \times 4) \\ &= 768.4 \text{ mm}^2 \end{aligned}$$

$$= \frac{25000}{768.4} \times 4$$

$$\sigma_b = 130.1 \text{ Mpa.}$$

2.3 NUMERICAL RESULTS

Tabulated breaking stress values from numerical calculation

The Maximum breaking stresses present in T-joint weldment at the throat thickness with the gap variation are given in table1 and the variation of Maximum breaking stress with respect to gap is also shown in Table. 4.1. Where 30° , 45° & 60° chamfer is provided on the vertical plate by varying the gap of 0.3, 0.6 and 0.9mm.

Gap between parent plats(mm)	Breaking stress for 25KN(Mpa)		
	30°	45°	60°
0.3	130.10	188.04	222.20
0.6	130.34	188.50	223.41
0.9	130.60	189.90	224.60

Table.2.1 Numerical results for breaking stress with different angle and gap between parent materials

3. EXPERIMENTAL ANALYSIS

3.1 OPTIMIZATION

Optimization is used to reducing the time, cost of weld simulation parameters [10,11]. Choosing welding process necessary to obtain the weld bed shape because of due to weld current, weld speed, arc voltage and its time consuming and this effects of weld parameters using optimization [12]. Defined as the process of finding the conditions that give the minimum or maximum value of a function, where the function defines the effort

required or the desired benefit. The act of obtaining best result under the given circumstances. Design, construction and maintenance of engineering systems involve decision making both at the managerial and the technological level.

3.2 TAGUCHI TECHNIQUE

Taguchi is the one of the optimization technique. Dr.Taguchi of Nippon telephones and telegraph company, Japan has developed a method based on orthogonal array experiments which gives much reduced “variance” for the experiment with optimum settings control variables [12]. Thus the marriage of Design of Experiments with optimization variables to obtain BEST results is achieved in the Taguchi method. “Orthogonal Array” provide a set of well balanced experiments & Dr.Taguchi’s signal-to-Noise ratios(S/N), which are log functions of desired output, serve as objective functions for optimization, help in data analysis and prediction of optimum results.

4. EXPERIMENTAL WORK

In this process TIG welding process is used with AISI1020 low carbon steel (parent material) and cu (filler material) with dimensions (100x50x5) mm.

A welded T-joint is considered for determination of breaking strength is shown in fig.4.1. For experimental testing process, two vertical plates are welded

with fillet weld at base plate top and bottom side having the cross section of 100 X 50 X 5 mm and 60 X 50 X 5 mm thick. The fillet weld size on bottom side is of 8 mm which is more than the top side fillet weld size of 4 mm, for studying the breaking strength of top side T-joint weld which is having less strength than the strength of bottom side of fillet weld.



Fig 4.1 welded T-joint material by Tungsten Inert Gas welding process

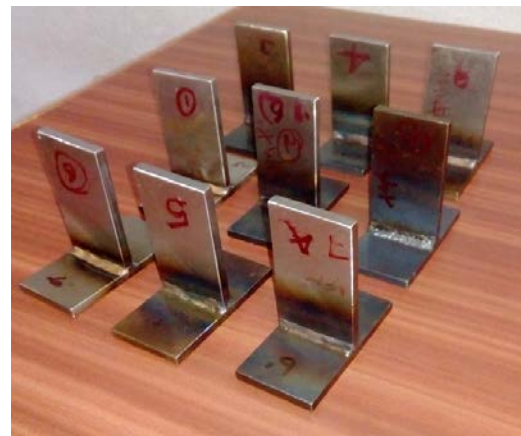


Fig.4.2 Nine types of weld T- joint welds by TIG welding process

4.1 DESIGN OF EXPERIMENT

Taguchi's designs aimed to allow greater understanding of variation than did many of the traditional designs. Optimizing process parameters of MIG

welding process and compare the experimental result with FEA for optimizing parameter by using (DOE) technique[13]. Taguchi contended that conventional sampling is deficient here as there is no way of obtaining a random sample of future conditions. Taguchi proposed extending each experiment with an orthogonal array should replicate the random environment in which the experiment would function.

Ex. No	Gap (mm)	Arc force (mm/s)	Angle (degree)
1	0.3	5	45
2	0.3	10	53
3	0.3	15	60
4	0.6	5	53
5	0.6	10	60
6	0.6	15	45
7	0.9	5	60
8	0.9	10	45
9	0.9	15	53

Table4.1 Experimental layout using L₉ Orthogonal Array

Welding process parameters

Parameters	Level-1	Level-2	Level-3
Gap (mm)	0.3	0.6	0.9
Arc force (mm/s)	5	10	15
Angle Degree	45	53	60

Table 4.2 Process parameters

ULTIMATE TENSILE TESTING



Fig4.3 Universal testing machine (UTM)

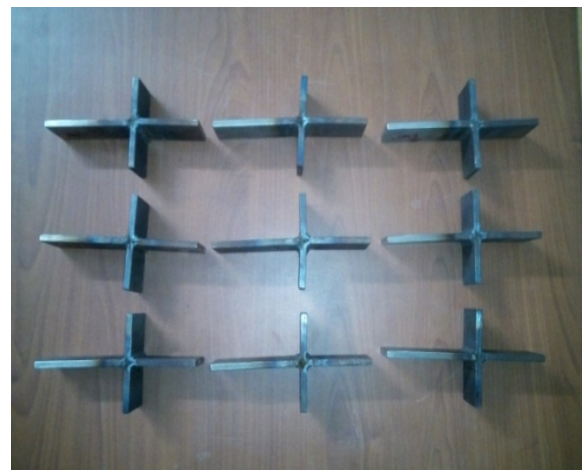


Fig 4.4 Nine types of t-joint weld section for testing purpose



Fig 4.5 Testing before and after breaking

199.17 Mpa for 45° and 1mm gap between the parent material.

2. 25KN load, $\theta = 60^\circ$ and 0.3mm gap

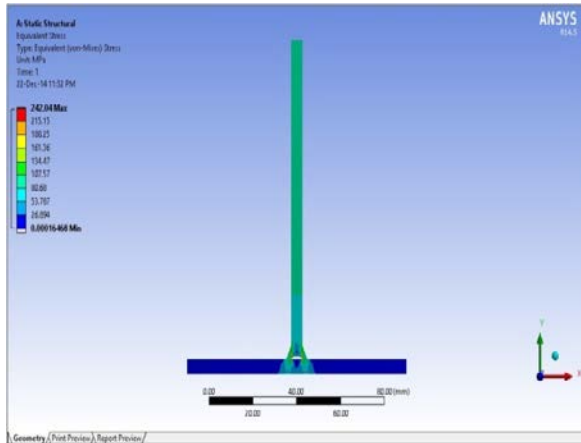


Fig5.2 Equivalent von-misses stress for 60° degree and 0.3mm gap

3. 25KN load, $\theta = 30^\circ$ and 0.3mm gap

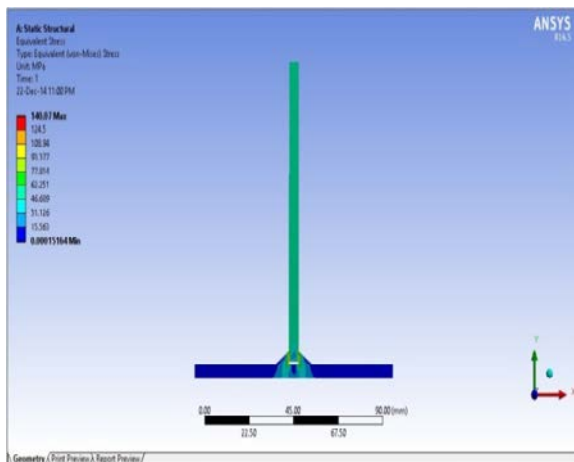


Fig5.3 Equivalent von-misses stress for 30° and 0.3mm gap

5.3 ANALYSIS RESULT

FE analysis is also carried out by considering the chamfer on vertical plate. The Maximum von-misses stresses present in T-joint weldment at the throat thickness with gap variation are carried out

and the variation of Maximum breaking stress with respect to gap and angle is also shown in Table.5.1. Where 30°, 45° & 60° chamfer is provided on the vertical plate by varying the gap of 0.3, 0.6 and 0.9mm.

Gap between parent plats(mm)	Breaking stress for 25KN(Mpa)		
	30°	45°	60°
0.3	140.07	197.17	242.04
0.6	142.89	197.91	247.02
0.9	149.12	205.09	252.73

Table.5.1 Analysis results for Von misses stress with different angle and gap

The above table shows the breaking stress for gap between parent plates. The maximum breaking stress 252.73Mpa for 60° angle with 0.9mm gap welded section. From the analytical and numerical results the equivalent von misses stress 80% approximately equal. The FE analysis of T-joint weld for the same geometry revealed the maximum Von-misses stress of 252.73Mpa it’s approximately equal to numerical maximum breaking stress of 224.6Mpa.

6. RESULTS AND DISCUSSION

- 1) The finite element and numerical analysis results of equivalent von misses stress are carried out and it’s approximately equal to the numerical breaking stress. The FE analysis of T-welded joint for the same geometry revealed the maximum Von-misses stress of 252.73Mpa it’s approximately

equal to numerical maximum breaking strength of 224.6Mpa.

0.9 mm and 60°	NUMERICAL RESULT	FEA RESULT
Breaking stress	224.6Mpa	252.73Mpa

- 2) From the finite element analysis maximum breaking stress is 252.73Mpa (0.9mm gap and 60°) and minimum breaking stress is 140Mpa (0.3mm gap and 30°).
- 3) The experimental and finite element results of breaking stress are carried out. The maximum breaking stress for experimental result is 236Mpa its approximately equal to the same geometry revealed the maximum Von-misses stress of 242Mpa.

0.3 mm and 60°	EXPERIMENTAL RESULT	FEA RESULT
Breaking stress	236.2Mpa	242.04Mpa

- 4) From the experimental analysis maximum breaking stress is 232Mpa (0.3mm gap and 60°) and minimum breaking stress is 151Mpa (0.3mm gap and 53°).
- 5) The optimization of T-joint weld is successfully carried out both analytical and experimentally.

6.1 TESTING RESULTS

Ex.No	Gap (mm)	Arc force	Angle (degree)	Breaking load
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		(mm/s)		(KN)
1	0.3	5	45	22.4
2	0.3	10	53	23.5
3	0.3	15	60	26.5
4	0.6	5	53	21.7
5	0.6	10	60	22.3
6	0.6	15	45	19.2
7	0.9	5	60	20.2
8	0.9	10	45	18.3
9	0.9	15	53	17

Table 6.1 Breaking load for fillet weld materials by UTM

The table 6.1 represents the breaking loads for T-joint welds with varies gap and angle. From this testing result carried out a maximum breaking load 26.5KN for 0.3 mm gap and 60° angle of fillet weld by taguchi method. Using this breaking load maximum breaking stress can be calculated as follows.

Maximum breaking load = 26.5 KN

Maximum breaking stress = 236.2 Mpa
for 0.3mm and 60° angle.

6.2 SAMPLE REPORT

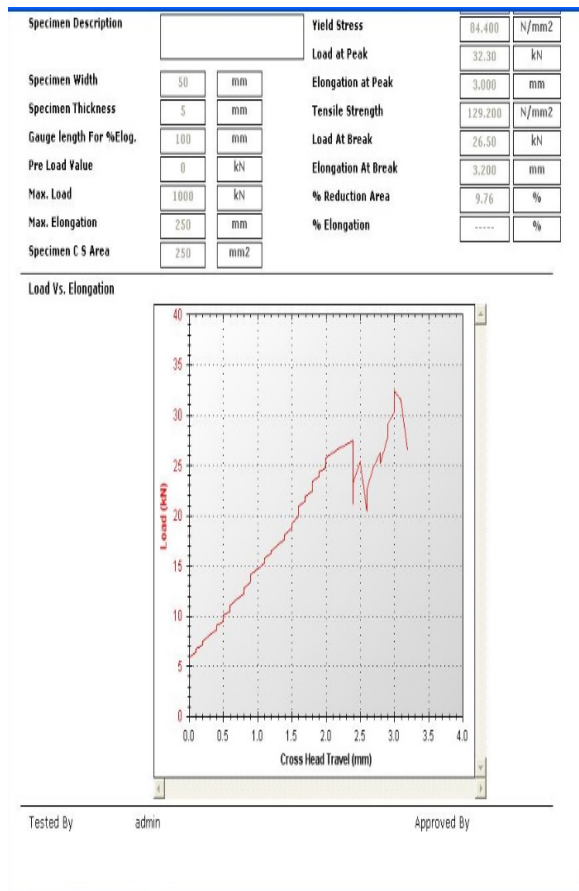


Fig 6.1 Sample report for maximum breaking load

CONCLUSION

The finite element analysis is used in this work to evaluate the deformation breaking stress of weld T-joint to restrict the weldment failure (using low carbon steel as a base metal and copper filler material). Static stress analysis performed on the weldment under tensile load revealed the maximum Von-misses stress with respect to the gap between base plates using ANSYS work bench 14.5. The design and analysis of welded T-joint has been done successfully.

The experimental analysis is carried out by using taguchi technique to evaluate the maximum breaking stress and results are compared with FE analysis and

both are approximately acceptable. The conclusion obtained by this project work are summarized below,

- The 60° angle parameter is gives better breaking stress results in experimental & analytical compared then 30° and 45°.
- The experimental investigation shows the 0.3 gap between parent material with 60° angle gives a maximum breaking stress.
- If the gap is increased means breaking stress will gradually decreased by experimental analysis.
- Low carbon steel AISI1020 is gives fine welding with copper and it's did not create any crack or flows during welding process.
- Arc force 15mm/s is giving a fine welding and increase the weldability of the T-joint.
- Using this optimized angle and gap between parent material is restrict the weldment failure.

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